# Worksheet - Open Fencing - Wind Loading

Site Location:					
Customer:  Site and Geometrical Variables					
IBC ASCE 7	Risk Category	Frost Depth ft			
Basic Wind Speed, V <sub>w</sub> = mpl	า				
Wind Pressure, q <sub>w</sub> = psf					
Exposure Category	Topographical Factor, K <sub>zt</sub> =				
Site Elevation, Z <sub>e</sub> = ft	Elevation Factor, K <sub>e</sub> =				
Height of fence, h =ft	Gap at bottom of fence, g =	ft(zero if no gap)			
Height of fencing material, s = h - g =	ft				

Velocity Pressure Exposure Coefficient, K<sub>z</sub> = \_\_\_\_\_

## Wind & Axial Loading

Fence Run #\_\_\_\_

Length of Fence, B = \_\_\_\_\_ ft

Post spacing, L = \_\_\_\_ ft

Solidity Ratio,  $\varepsilon =$ \_\_\_\_\_

Inverted Fence Opening Reduction Factor,  $R_{1w} = 1.0$ 

Force Height Adjustment Factor, F<sub>hw</sub> = 1.0

Wind Force Coefficient,  $C_{fw} =$ \_\_\_\_\_

Expected Post Diameter or Width,  $\mathcal{O}_p = \underline{\hspace{1cm}}$  in

Top Rail Diameter or Width,  $\mathcal{O}_r = \underline{\hspace{1cm}}$  in

Mid Rail Diameter or Width,  $\mathcal{O}_p = \underline{\hspace{1cm}}$  in

 $(\mathcal{O}_r \& \mathcal{O}_m - \text{set to Zero if not applicable for rails})$ 

Wind Area of Post, 
$$A_p = \mathcal{O}_p / 12 \times h = \underline{\hspace{1cm}} \div 12 \times \underline{\hspace{1cm}} = \underline{\hspace{1cm}} ft^2$$
 (A<sub>p</sub> = 0 for solid / mostly solid fencing)  $\mathcal{O}_p$  h  $A_p$ 

Wind Area of Rails,  $A_r = (\emptyset_r / 12) \times 2 \times L + (\emptyset_m / 12) \times L$  ( $A_r = 0$  if no rails)

$$A_r = ( _{O_r} \div 12 \times 2 \times _{D_r} ) + ( _{O_m} \div 12 \times _{D_r} ) = _{A_r} ft^2$$

Wind area tributary to the post,  $A_w = \epsilon s L + A_p + A_r = \underline{\qquad} \times \underline{\qquad} \times \underline{\qquad} + \underline{\qquad} + \underline{\qquad} = \underline{\qquad} ft^2$ 

Dead Load of fencing materials, D<sub>m</sub> \_\_\_\_\_ psf

# **Lateral and Axial Forces for Wind Loading**

Minimum wind force to the post,  $f_{min}$  = (0.6) 16.0  $A_w$  = 9.6 × \_\_\_\_ = \_\_\_\_ | bs  $A_w$   $f_{min}$ 

Calculated Wind Force to the post,  $f_w = q_w K_z K_{zt} K_e R_{1w} F_{hw} C_{fw} A_w$ 

$$f_w = \underbrace{\hspace{1cm} \times \hspace{1cm} \times \hspace{$$

Maximum wind force to the post,  $f_w' = \text{maximum value of either } f_{\text{mim}} \text{ or } f_w = \underline{\qquad} \text{lbs}$ 

Axial force supported by the post,  $p_a = D_w s L$ 

$$p_w = \underline{\hspace{1cm}} \times \underline{\hspace{1cm}} \times \underline{\hspace{1cm}} = \underline{\hspace{1cm}} Ibs$$

 $5 \times p_w =$  \_\_\_\_\_ lbs (used for stability check)

#### **Post Selection**

Using the size of the desired post and the Fence Height, h, look through the post charts for post types that have an  $F_a$  value larger than the  $f_w$  value, and a  $P_a$  value larger than the  $p_w$  value. If the post has an \* next to the  $P_a$  value, only use it if the  $P_a$  value is  $\geq 5 \times p_w$  due to stability requirements.

Put in the O.D or size, post type, weight per foot,  $D_p$  and fence height, h and calculate  $p_w$  to include the weight of the post. Add any additional weight if needed.

fw' / Fa is the bending strength ratio for Wind

pw' / Pa is the axial strength ratio for Wind

If the sum of the bending strength and axial strength ratios are  $\leq$  1.0, the post is acceptable.

O.D.	Post Type	D <sub>p</sub> (lb/f)	h (ft)	$p_w' = p_w + (D_p \times h)$	
				p <sub>w</sub> =	
Wind					
f <sub>w</sub> ' =					
F <sub>a</sub> =	_		Pa =	-	F <sub>a</sub> P <sub>a</sub>

O.D.	Post Type	D <sub>p</sub> (lb/f)	h (ft)	$p_w' = p_w + (D_p \times h)$	
				p <sub>w</sub> ' =	
	Wind				
f <sub>w</sub> ' = = <u>f<sub>w</sub>' _ p<sub>w</sub>' = </u>					
F <sub>a</sub> =			P <sub>a</sub> =	_	F <sub>a</sub> P <sub>a</sub>

O.D.	Post Type	D <sub>p</sub> (lb/f)	h (ft)	$p_w' = p_w + (D_p \times h)$	
				p <sub>w</sub> 1 =	
Wind					
f <sub>w</sub> ' =					
F <sub>a</sub> =	_		$P_a =$	_	F <sub>a</sub> P <sub>a</sub>

## Footing Sizing (non-constrained footings)

Design Footing Depth, D = \_\_\_\_\_ft

Footing Diameter, b = \_\_\_\_\_ft

Lateral Bearing Pressure per foot of depth, S = \_\_\_\_ psf / ft per geotechnical analysis or table 1806.2

Maximum Wind Force, P = f<sub>w</sub>' = \_\_\_\_\_ lbs Post Height, h = \_\_\_\_ ft

Modifier for Isolated Posts, M = 2.0

per IBC §1086.3.4

Allowable Lateral Soil Bearing Pressure for non-constrained footings, S₁ = ⅓ D S M

$$S_1 = \frac{1}{3} \times \underline{\hspace{1cm}} \times \underline{\hspace{1cm}} \times 2.0 = \underline{\hspace{1cm}} \text{psf}$$
 per IBC §1807.3.2.1

Soil Bearing Factor,  $A = 2.34 P/(S_1 b)$ 

per IBC §1807.3.2.1

$$A = 2.34 \times _{P} \div (_{S_1} \times _{b}) = _{A}$$

Minimum Depth,  $d = \frac{1}{2} A \left(1 + \sqrt{1 + \frac{4.36 \frac{1}{2} h}{A}}\right)$  per Eq. 18-1, modified for fencing

$$d = \frac{1}{2} \times \underline{\qquad} \times (1 + \sqrt{1 + (4.36 \times \frac{1}{2} \times \underline{\qquad} \div \underline{\qquad})) = \underline{\qquad} ft$$

Area of the bottom of the footing,  $A_f = \pi (\frac{1}{2} b)^2 = 3.14 \times (\frac{1}{2} \times \underline{\phantom{a}})^2 = \underline{\phantom{a}}_{A_f} ft^2$ 

Footing Volume,  $V = A_f D = \underline{\qquad} \times \underline{\qquad} = \underline{\qquad} ft^3$ 

Weight of footing,  $D_f = 150 \text{ V} = 150 \text{ x} = 150 \text{ J} = 150 \text{ m}$  lbs (Typical Concrete weight is 150 lbs / ft<sup>3</sup>)

Axial Dead Load,  $D_{max} = D_f + p_w$ 

$$D_{max} = \underline{\qquad} + \underline{\qquad} = \underline{\qquad} lbs$$

Maximum Vertical Foundation Pressure,  $S_y = \underline{\phantom{0}}$  psf per geotechnical analysis or table 1806.2

Maximum Axial Pressure on the soil,  $s_y = D_{max} / A_f = \underline{\qquad} \div \underline{\qquad} = \underline{\qquad} psf$ 

Actual to Allowable Soil Strength Ratio,  $s_y$  /  $S_y$  = \_\_\_\_  $\div$  \_\_\_ = \_\_\_  $\le$  1.0 is OK

 $s_y$  /  $S_y$  must be less than 1.0. If not, start over with a larger footing diameter, b